# The use of spunbonded geotextile in railway track renewal St. Petersburg-Moscow

E.S. ASHPIZ, University of Transport Engineers, Moscow, Russia R. DIEDERICH & C. KOSLOWSKI, DuPont de Nemours, Luxembourg

ABSTRACT: A research project was performed in order to improve and renew an existing railway line to handle higher speed trains. Old contaminated ballast layer has been removed, cleaned and re-installed after laying a thermally bonded geotextile with high initial modulus as separation and stabilisation layer. The operation has been made with specialised equipment without removing the track. After one and after five years the track has been opened and the performance and behavior of the geotextile has been analysed. The research showed that the proposed solution proved sufficient reliability of the design and of the selected geotextile.

## 1. INTRODUCTION

The railroad St. Petersburg-Moscow (Russia) founded 150 years ago with a length of 650 km was being renewed to handle higher speed trains. After reconstruction, the line was used for passenger transportation as well as freight cargos with axle load up to 230 kN/axle.

These load conditions demanded serious improvement of the track substructure. During the track's lifetime a mass of old ballast material with a thickness of up to 1,5m under the sleeper had accumulated. The old ballast consists mainly of crushed stone of 25-60 mm and contains up to 40 % of small particles, 5-6 % of which are under 0,1mm. Due to dynamic loads these small particles penetrated into the ballast layer and caused insufficient strength of the ballast. This pumping effect occurred mostly in spring and after heavy rains.

Therefore one of the objectives of the track renewal was reinforcement of roadbed and ballast section to provide longterm stability of the track.

# 2. TRACK RENEWAL OPERATION

For reaching the required track stability it was decided to clean the old ballast to a depth of 0.4 - 0.45 m under the sleepers over the whole line and to install a separation layer between cleaned ballast and old ballast. In total around 800 km of geotextile was installed.

## 2.1. Installation

The line renewal operations were done during 8 hours daily. After that, the line was opened again for traffic. Crushed stone cleaning and geotextile laying were performed using specialised equipment without removing the track. The geotextile was laid on the top of the old ballast and covered with cleaned crushed stone without additional protective layer.

In order to drain the water, the edge of the old removed ballast was cut in a way that it formed an incline of 4%.

Figure 1. Principle of installation of the geotextile and new ballast layer



Figure 2. Track renewal with specialised equipment



#### 2.2. Product selection

A thermally spunbonded nonwoven geotextile of 100% polypropylene with high initial modulus and high energy absorption resistance was selected. The pre-compressed structure with minimal thickness allowed a maximum coil length with fixed roll diameter.

Table 1. Typar® 3857 Main properties

	Standard	Unit	
		measure	
Breaking load	EN ISO 10319	kN/m	20.5
Elongation at rupture	EN ISO 10319	%	70
Load at 5% elongation	EN ISO 10319	kN/m	9.8
Energy absorption	EN ISO 10319	kJ/m <sup>2</sup>	10
CBR puncture	EN 12236	N	3130
Permeability coefficient at 20 kN/m <sup>2</sup>	SN 640550	10 <sup>-4</sup> m/s	2.7
Surface density	EN 965	g/m <sup>2</sup>	290
Thickness under the load of 2 kN/m <sup>2</sup>	EN 964-1	mm	0.75
Coil length		m	110

## 3. EVALUATION OF PERFORMANCE

#### 3.1. Pilot site build-up

As the concern was raised that without additional protective sand layer damage could occur on the geotextile, a pilot site was constructed on the line St. Petersburg - Moscow. Geotextiles were installed according to six different build-ups.

1. Cleaned crushed stone – 1 layer of selected geotextile – old ballast.

2. Cleaned crushed stone – protective layer of sandy gravel - 1 layer of selected geotextile – old ballast.

3. Cleaned crushed stone – protective sand layer – 1 layer of selected geotextile – old ballast.

4. Cleaned crushed stone – 1 layer of selected geotextile – protective sand layer – old ballast.

5. Cleaned crushed stone -2 layers of selected geotextile - old ballast.

6. Cleaned crushed stone -1 layer of needlepunched geotextile  $400g/m^2 - old$  ballast.

After one year of operation a sample of the geotextile was excavated on the site and the ballast was examined for contamination. Geotextile samples were tested in a laboratory and changes in its area weight, moisture content and damage resistance were analysed.

#### 3.2. Discussion of results

The additional sand layer improved the geotextile performance. A sand layer below the geotextile provided the additional advantage of a plane surface for the installation. It was noticed that the geotextile was under tension, which shows a possible stabilisation effect of the geotextile.

The first test took place after one year of operation and the second in 2001 after five years of service.

Only some minor puncture holes of 1-2 mm were found, which represented only 0.2 % of the total surface area of the geotextile. The lowest result on moisture and soil content in the structure was found with additional sand layers. Without additional sand layer a much higher content has been found for the thicker needlepunched product compared to the selected thermal bonded product.

Table 2. Geotextile parameter after one year of use in the railway track

Nº			Area weight, g/m <sup>2</sup>			Moisture content,	
			new	wet	dry	Soil content	%
1	Geotext	tile only	290	828	641	351	29.1
2	Geot	extile	290	541	442	152	22.4
	under sandy gravel layer						
3	Geot	extile	290	486	443	153	9.6
	under sand layer						
4	Geotextile		290	581	511	221	13.7
	above sand layer						
5	Geotextile	Upper layer	290	763	600	310	27.2
	2 layer	Lower layer	290	780	632	342	23.4
6	Needle-punched, 1 layer only		400	1468	1035	635	41.9

#### 4. EXCAVATION AFTER 5 YEARS

After 5 years of service life the track was opened on several sections in order to determine the performance of the geotextile. Samples were excavated and tested to determine area weight, breaking load and water permeability.

Figure 3. Excavation from under the track



#### Figure 4. Excavated sample of geotextile with some old ballast



#### 4.1. Retained mechanical properties

After 5 years of service life the total damage surface was 0.3 % compared to 0.2 % after one year. The retained strength after one year was 74 % and after 5 years still 72 % with a remaining elongation of up to 30%.

The decrease in material strength as well as most of the damages occurred in the beginning and did not further change with time. Initial modulus did not change.

Figures 5 and 6 show the stress-strain curves of the geotextile after 5 years at different locations compared to the initial results. The tensile strength test was performed on 5cm wide samples. The geotextile showed no decrease in puncture strength. Puncture strength after 5 years of service life was 1281 N compared to 1280 N of initial strength.

Figure 5. Typar® 3857 stress-strain-curve (MD)



Figure 6. Typar<sup>®</sup> 3857 stress-strain curve (XD)



Table 3. Tensile strength and elongation after 5 years [N/5cm]

km	Sample	Pmax, H	Elong. max, %	Pmax, H	Elong. max, %
578 km	1	540	14.9	505	13.1
	2	580	11.6	526	10.4
	3	660	24.1	612	27.1
	4	455	16.0	640	19.1
	5	668	22.9	830	41.3
	Mean	581	17.9	623	22.2
	STDEV	89	5.4	129	12.5
573 km	1	420	11.1	614	18.9
	2	373	9.8	570	24.6
	3	436	8.2	750	27.9
	4	459	11.7	720	23.8
	5	528	16.7	720	24.6
	Mean	443	11.5	675	23.9
	STDEV	57	3.2	78	3.2
553 km	1	654	23.0	694	22.6
	2	761	22.6	942	41.4
	3	466	10.4	720	30.8
	4	672	24.6	643	15.3
	5	738	27.3	834	34.4
	Mean	658	21.6	767	28.9
	STDEV	116	6.5	120	10.2
391 km	1	720	20.5	550	18.0
	2	560	13.9	576	23.8
	3	479	12.3	555	19.7
	4	620	20.9	780	37.7
	5	515	13.1	725	28.5
	Mean	579	16.2	637	25.6
	STDEV	95	4.2	107	7.9

## 4.2. Retained hydraulic properties

Some contamination of the geotextiles was noticed after extraction. Tests of the un-cleaned geotextile with ballast showed that the water permeability of the whole structure decreased only 1.5 times. The conditions found on the track at various sections confirmed that the existing decrease in water permeability of the geotextile did not affect humidity conditions of the structure as most part of incoming water is drained in the ballast layer on top of the geotextile. During extraction it was found that the moisture content of the ballast under the geotextile was 1-2% less than above the geotextile.

It was clearly visible that the contamination was mainly coming from the top of the structure due to abrasion of ballast and rain falls. Only minor contamination was found on the bottom part of the geotextile.

## 5. STABILISING EFFECT

During extraction it was found that the geotextile was stretched which shows that it functioned also as a stabilisation layer. In order to evaluate this stabilising effect of the geotextile, load cells were installed under the geotextile layer below the track axis, below the sleeper butt, on rail axis between sleepers and on rail axis under sleeper. In Russia similar measurements were repeatedly made in the ballast without geotextile. Based on these measurements in the depth of 0.4 - 0.5 m under the sleeper it was found that regardless of rolling stock unit and sleeper type, stress reduction factor on sleeper axis amounts to Ko/p= 0.33 and stress reduction factor on sleeper butt amounts to Km/p= 0.61. Analysing data from table 3 in comparison with coefficients for standard construction without geotextile one can conclude that

for all rolling stock units load balancing has occurred that demonstrates the stabilising effect of the used geotextile. Surface load balancing was the largest in case of passenger trains with lowest axle load and highest speed.

Table 4. Stress reduction factors on the ground under geotextile in cross-section.

Rolling stock unit	Axle load,	Speed,	Stress reduction factors		
	kN/axle	km/h	on track axis	on sleeper butt	on tie space
Freight locomotive	245	70	0.53	0.78	0.82
Freight car	230	70	0.52	0.76	0.83
Passenger locomotive	191	110	0.67	0.84	0.90
		160	0.63	0.85	1.00
Passenger car	157	110	0.79	0.86	0.97
		160	0.67	0.69	0.83
High-speed electric	167	175	0.68	0.75	0.92
train					

## 6. CONCLUSIONS

The tests confirmed that the proposed solution proved sufficient reliability of the design with the selected geotextile in the ballast without protective layers.

- Minor damage that had no influence on track functionality was found on the geotextile

- Geotextile works as a separating layer and prevents

contamination of the new ballast

- Contamination of the geotextile had little influence on the

drainage capacity of the whole system

- Contamination and damage occurs in the beginning; it becomes stable with time

- The selected geotexile with high initial modulus stabilised the whole structure

Track measurement cars are passing twice a month. According to these measurements, track sections stabilised with the selected geotextile remain flat after several years and ensure train operation on required speed and axle loads.

## REFERENCES

- Central Scientific & Research Institute of Ministry of Rails of Russian Federation, 1972. Stress and elastic deformations in the ballast bed under trains impact. Moscow: Publishing house "Transport".
- Diederich, R. 2000. Evaluation of Installation Damage of Geotextiles. A Correlation to Index Tests, YiChang China 2000, Fifth Conference on Geosynthetics
- Rails and Engineering Department, Ministry of Rails of Russian Federation, 1999. Technical guideline for the application of foamed polystyrene and geotextile in railway ballast bed without removal of rails and sleepers. Moscow.
- Research report N 84/97, 1997. Laboratory evaluation of Russian geotextiles for the possible application as separation layer in the railway St. Petersburg-Moscow. Moscow: University Of Transport Engineers.
- Research report N 06/97-z, 1998. Observations on the rails stability, conditions of ballast bed and protection layers on the test repair department. Moscow: Research & Production Company "Geonika-PM".
- Research report N 03/98-z, 1998. Observations on the rails stability, conditions of ballast bed and protection layers on the test repair department. Moscow: Research & Production Company "Geonika-PM".
- Research report N 68/99, 1999. Measurements of stress and deformations in the ballast bed on the high speed test section on a stable sub-base. Moscow: University Of Transport Engineers.
- Watn, Eiksund, Knutson. 1998. Deformations and Damage of Nonwoven Geotextiles in Road Construction, Atlanta 1998, Sixth International Conference on Geosynthetics